



## Journal Article

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# Response analysis of electron attachment rates to $\text{C}_3\text{F}_8$ and $\text{SF}_6$ in buffer gases

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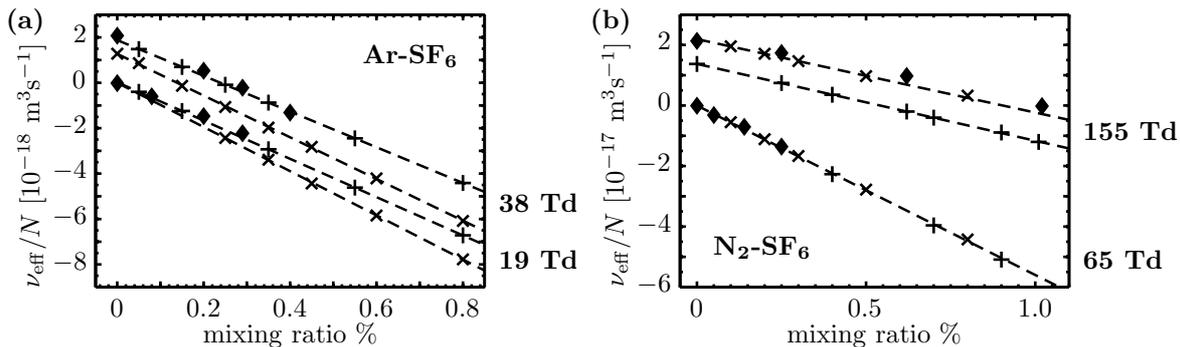
**Abstract.** Electron swarm methods are applied for investigating the effects of small amounts ( $\leq 1.5\%$ ) of a strongly electronegative sample gas in the buffer gases Ar,  $\text{N}_2$  or  $\text{CO}_2$ . A pulsed Townsend method, a Monte Carlo swarm method, and a solution of the Boltzmann equation are used to determine the effective ionization rate constants of the gas mixtures. The sensitivity of the effective ionization rate constant to changes of the mixing ratio is evaluated. Our methods are benchmarked with the analysis of Ar- $\text{SF}_6$  and  $\text{N}_2$ - $\text{SF}_6$  mixtures, and subsequently used for the analysis of gas mixtures containing  $\text{C}_3\text{F}_8$ . The results based on the recommended  $\text{C}_3\text{F}_8$  cross sections are shown to be inconsistent with the experimental data for  $\text{N}_2$ - $\text{C}_3\text{F}_8$  and  $\text{CO}_2$ - $\text{C}_3\text{F}_8$  mixtures.

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## 1. Introduction

Gas mixtures containing strongly electronegative molecules are the medium for many industrial plasma processes, and for high voltage insulation and switching. Both these application domains require knowledge of the electron attachment parameters of electronegative molecules [1, 2]. One can investigate the attachment parameters of a sample molecule by means of swarm parameter measurements in buffer gases [3, 4, 5], when the relative concentration (mixing ratio)  $k$  of the sample molecule is small. In buffer gases with well known electron energy distribution (EEDF), like Ar,  $\text{N}_2$  or  $\text{CO}_2$ , such experimental results are important for assessing the attachment cross sections of a sample molecule [3, 5, 6]. These experimental data can be applied more generally and readily, when the experimental technique achieves a separation between the swarm parameters of the buffer gas and the effects of the sample gas. For example, the swarm parameters of gas mixtures were evaluated for the rate constants of electron attachment to a sample molecule [3, 7]. However, these analyses were limited to such values of the reduced electric field strength  $E/N$  where ionization could be neglected. We aim for applying a similar technique also near the critical field strength  $(E/N)_{\text{crit}}$ , where the



**Figure 1.** Measurements ( $\blacklozenge$ ) of the effective ionization rate constant, and the values ( $+$ ) calculated by a Boltzmann solver [8] or ( $\times$ ) simulated by a Monte Carlo method [9] as a function of the mixing ratio of (a)  $SF_6$  in Ar, and (b)  $SF_6$  in  $N_2$ . The lines ( $- - -$ ) represent the linear trends of the simulated or calculated values.

ionization rate equals the attachment rate, because this ( $E/N$ )-range is of particular interest for high voltage insulation technology.

For certain mixtures of an electronegative gas and a buffer gas, and for particular values of  $E/N$ , a linear relation is apparent between  $k$  and the effective ionization rate constant  $\nu_{\text{eff}}/N$ . This is shown, for example, in figure 5 of [10] and figure 8 of [11]. Such a linear relation also appears in our measurements and in the results of two mutually independent numerical methods [8, 9], as one can note from the figures 1 and 6 of the present article.

Based on the assumption of a linear relation between  $\nu_{\text{eff}}/N$  and  $k$ , we attempt to develop a linear response technique as a more convenient method for investigating the electron attachment parameters of sample molecules. This technique shall be tested with  $SF_6$  which is a gas with well known parameter values [12].  $SF_6$  can therefore be considered as providing a benchmark [1, 13]. We compare our measurements to numerical results because experimental data are scarce in the parameter range of the present study [10, 11]. Subsequently, the linear response technique is applied for testing the attachment cross sections of octafluoropropane ( $C_3F_8$ ).

### 1.1. Octafluoropropane

Previous work on  $C_3F_8$  has been reviewed in [14, 15]. More recently, a new set of electron collision cross sections was derived from drift tube measurements [16], and the electron-impact dissociation cross sections were remeasured [17]. It is known that the electron attachment rate constant depends on the total gas density and the gas temperature. For 300 K and high total gas density,  $\sim 10^{26} \text{ m}^{-3}$ , the transient anion can be stabilized due to 3-body processes, and the non-dissociative attachment rate is comparable to the dissociative attachment rate. For higher temperatures  $> 500 \text{ K}$ , only dissociative attachment was observed [18]. In consequence, the dissociative attachment cross section for 300 K was derived by extrapolating results obtained at elevated temperature. The present study is made at intermediate gas density,  $\sim 10^{24} \text{ m}^{-3}$ , at about 300 K, where

our methods are not sensitive enough to detect a minor influence of density dependent processes. We argue that an independent test of the attachment cross sections is possible with the data of the present study.

## 2. Methods

### 2.1. Linear response technique

The effective ionization rate constant of a gas mixture  $(\nu_{\text{eff}}/N)_k$  with mixing ratio  $k$  is defined by the EEDF  $F_k(\varepsilon)$  and by the ionization and attachment cross sections of the sample gas,  $\sigma_i(\varepsilon)$  and  $\sigma_a(\varepsilon)$  respectively, and the ionization minus the attachment cross sections of the buffer gas  $\sigma_B(\varepsilon)$ , see also (10) in [8].

$$(\nu_{\text{eff}}/N)_k = \sqrt{\frac{2}{m_e}} \int_0^\infty \varepsilon \{(1-k)\sigma_B + k(\sigma_i - \sigma_a)\} F_k d\varepsilon, \quad (1)$$

where  $m_e$  is the electron mass and

$$\int_0^\infty \sqrt{\varepsilon} F_k d\varepsilon = 1.$$

We assume that  $F_k(\varepsilon)$  is very similar to the EEDF of the pure buffer gas  $F_B(\varepsilon)$ :

$$F_k \rightarrow F_B \text{ for small } k. \quad (2)$$

Then (1) resolves to

$$(\nu_{\text{eff}}/N)_k \approx (\nu_{\text{eff}}/N)_B - k \sqrt{\frac{2}{m_e}} \int_0^\infty \varepsilon \{\sigma_B - \sigma_i + \sigma_a\} F_B d\varepsilon \quad (3)$$

$$(\nu_{\text{eff}}/N)_k \approx (\nu_{\text{eff}}/N)_B - k r_{BA}, \quad (4)$$

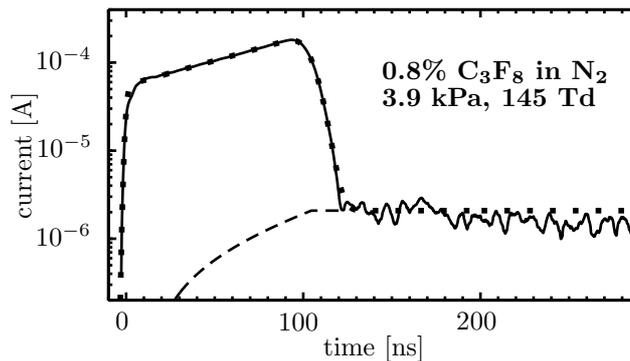
with the effective ionization rate constant of the pure buffer gas  $(\nu_{\text{eff}}/N)_B$ , and the linear response parameter  $r_{BA}$ , which constitutes a characteristic property of a particular combination of a buffer gas B and a sample gas A.

Equation (4) evaluates the sensitivity of  $\nu_{\text{eff}}/N$  on changes of  $k$ . It shall be used for obtaining  $r_{BA}$  as a function of  $E/N$  from calculated, simulated or measured  $\nu_{\text{eff}}/N$ . One expects  $r_{BA} > 0$  for the sample gases and the  $E/N$ -range of the present study because the term  $\sigma_a$  predominates in the convolution integral (3).

*2.1.1. Conditions for valid application.* Assumption (2) holds only if the sample gas does not perturb the momentum and energy balance of the electron swarm [6, 19]. Only then it is valid to apply (3) for an interpretation of the linear response parameters. Otherwise, a perturbation of  $F_B$  must be taken into account when making a connection between  $r_{BA}(E/N)$  and  $\sigma_a(\varepsilon)$ .

The influence of electron attachment on  $F_B$  can be neglected only if the attachment rate  $\nu_a$  is much smaller than the total energy transfer rate [19]

$$\nu_a \ll \frac{2m_e}{M} \nu_m + \sum_j \delta_j \nu_j, \quad (5)$$



**Figure 2.** Logarithmic plot of measured swarm drift current (—) and a fit (·····) of the swarm current model, which includes the ion current (---). The electrode spacing was  $d = 15$  mm.

where  $M$  is the effective mass of the gas constituents,  $\nu_m$  is the momentum transfer collision rate, and  $\nu_j$  are the rates of inelastic processes with fractional energy loss  $\delta_j$ .

In particular gas mixtures, condition (5) may be violated, and electron attachment to the sample gas can strongly affect  $F_B$  even for small  $k$ . For example, such perturbations of  $F_B$  were previously found at  $(E/N) \leq 20$  Td with 0.5%  $F_2$  in Ar [20], or with 0.1%  $NF_3$  in Ar [21]. For every particular combination of gases B-A, it is therefore necessary to test the range of  $E/N$  and  $k$  where a linear relation (4) can appear (see also sections 4.1.1 and 4.2.1).

## 2.2. Pulsed Townsend method

A pulsed Townsend (PT) electrical method is used. The experimental setup, its operation and the signal acquisition have not been modified since the original report [22]. The same methods are used here for recording the swarm drift currents and for evaluating the current waveforms. Four waveform parameters are obtained by fitting expressions derived from the usual swarm model [22] to the observed swarm drift currents:

- initial electron number
- swarm transit time  $T$
- effective ionization rate  $\nu_{\text{eff}}$
- bulk diffusion time constant  $\tau_D$

These waveform parameters are treated by normalization techniques [22] in order to obtain  $\nu_{\text{eff}}/N$  and the bulk drift velocity  $w$ .

In the parameter range of the present study, the waveforms and the modelled swarm currents almost coincide. Figure 2 shows an excellent agreement between the measured and calculated currents.

### 2.3. Numerical methods and cross sections

For *simulating* electron transport parameters, we use a Monte Carlo (MC) method (Magboltz [9] version 9.0.1). The simulation settings were:  $4 \times 10^8$  real collisions, total gas pressure 75 torr and temperature 297 K. Magboltz uses Itoh's cross section set for  $SF_6$  [23], and proprietary sets for Ar,  $N_2$ ,  $CO_2$  and  $C_3F_8$ . We note that the proprietary dissociative attachment cross section of  $C_3F_8$  closely corresponds to  $0.85 \times$  the recommended cross section [14].

For *calculating* electron transport data, we use a solver (Bolsig+ [8] version 11.2011) for the 2-term expanded Boltzmann equation (BE) with a cross section database (SIGLO [24] version 11.2011). It includes Phelps' cross section sets for Ar and  $N_2$  tested in [8], Morgan's set for  $CO_2$ , and Phelps' set for  $SF_6$  [25]. The solver settings were: Precision  $10^{-13}$ , Convergence  $10^{-5}$ , Iterations 100, gas temperature 297 K, temporal growth model, equal energy sharing after ionization.

There are well known limitations of using 2-term BE methods for testing cross sections [5]. However, in the  $(E/N)$ -range under study, we argue that the 2-term BE method yields rate constants with satisfactory precision, provided that an accurate cross section set is available. It must be emphasized that the BE and MC methods are entirely different, and that their results are mutually independent because they are based on different cross section sets. Our choice of numerical methods and cross sections was made in order to provide disparate reference data for  $SF_6$ -mixtures.

## 3. Results

The present work concerns binary mixtures of one sample gas,  $SF_6$  or  $C_3F_8$ , and one buffer gas, Ar,  $N_2$  or  $CO_2$ . The purity of the gases and the mixing ratios under investigation are summarized in table 1. Table 2 specifies the ranges of total gas pressure for the measurements. We use the swarm parameters of  $N_2$  and  $CO_2$  from our previous study [22]. The data for Ar are given in table A1.

### 3.1. Mixture preparation

Gas mixtures were prepared directly in the experimental vacuum vessel which has a base pressure  $< 10^{-5}$  Pa. After the vessel had been vented with the buffer gas B, the sample gas A was filled with the desired partial pressure. Then B was added to reach the desired total pressure. Gas pressure and temperature were continuously measured, and the total gas density  $N$  was determined at any time with uncertainty  $\pm 1\%$  in the relevant pressure range 50 Pa to 11 kPa. Gas mixtures with  $k < 0.5\%$  have been prepared starting from a mixture with  $k = 0.5\%$  by pumping out part of the mixture and then refilling B to the desired total pressure.

**Table 1.** Mixing ratios of the sample gases, and the measured critical field strength of the gas mixtures. The gas purity is stated in brackets (3.0  $\equiv$  99.9%).

buffer gas	SF <sub>6</sub> (3.0)		C <sub>3</sub> F <sub>8</sub> (4.0)	
	mixing ratio %	( $E/N$ ) <sub>crit</sub> (Td)	mixing ratio %	( $E/N$ ) <sub>crit</sub> (Td)
Ar (6.0)	0.08	30.5	0.17	25.3
	0.20*	37.5	0.25	32.7
	0.29	41.0	0.51*	34.2
	0.40	43.5	1.01	40.2
N <sub>2</sub> (5.0)	0.05		0.09	79.0
	0.14		0.37	93.8
	0.25*	129	0.81*	104
	0.62	144	1.51	113
	1.02	153		
CO <sub>2</sub> (5.0)			0.18	83.9
			0.27	85.1
			0.81*	92.5
			1.21	95.8

\* Tabulated swarm parameters given in the appendix.

### 3.2. Measurement parameters and procedures

The swarm parameter measurements were made at room temperature 293 to 300 K. After one measurement sequence was completed, the total pressure was reduced by pumping, and a subsequent measurement sequence was carried out. In this way the same gas mixture was investigated for 4 to 6 different  $N$ -values in the pressure range specified in table 2. The PT waveforms have been recorded for electrode spacings  $d = (17, 15, 13, 11)$  mm in the  $E/N$ -range of interest. The cumulative uncertainty of the ( $E/N$ )-values was  $\pm 1.5\%$ .

The PT waveforms have been evaluated for the swarm parameters  $\nu_{\text{eff}}/N$  and  $w$ . From the ( $\nu_{\text{eff}}/N$ )-data the critical field strength ( $E/N$ )<sub>crit</sub> was determined by interpolation. The ( $\nu_{\text{eff}}/N$ )-data of a pair of gases B-A with different  $k$  were plotted for selected values of  $E/N$ , as it is shown for example in figures 1 and 6. These plots served for checking the validity of a linear relation between  $\nu_{\text{eff}}/N$  and  $k$ ; refer to the discussion in sections 4.1.1 and 4.2.1. Finally, we applied (4) in order to obtain  $r_{\text{BA}}$ .

### 3.3. Data presentation

In table 2 the measurement parameters are specified for a gas mixture B-A, and the corresponding results are attributed.

**3.3.1.  $\nu_{\text{eff}}/N$ .** The results of the effective ionization rate constant are classified by two columns of table 2. These columns denote

**Table 2.** Overview of the parameter range of measurements, and a catalogue of figure numbers where the results are presented. Refer to section 3.3 for column descriptions.

buffer and sample gas	pressure (kPa)	$\nu_{\text{eff}}/N$		$r_{\text{BA}}$		
		overview (figure)	linearity (figure)	$(E/N)$ -range (Td)	$\langle \varepsilon \rangle$ -range (eV)	plot (figure)
Ar/ $SF_6$	2 – 8	3	1(a)	19 – 43	5.51 – 6.00	5
$N_2/SF_6$	2 – 8	4	1(b)	40 – 165	1.11 – 4.27	5
Ar/ $C_3F_8$	2 – 8		6(a)	22 – 46	5.61 – 6.06	7
$N_2/C_3F_8$	2 – 10.5		6(b)	20 – 150	1.03 – 3.85	7
$CO_2/C_3F_8$	2 – 9		6(c)	28 – 116	1.07 – 4.45	7

- (i) a figure number where our measurements of  $\nu_{\text{eff}}/N$  are plotted together with reference data.
- (ii) a figure number where  $\nu_{\text{eff}}/N$  was plotted as a function of  $k$  for selected values of  $E/N$ .

3.3.2.  $r_{\text{BA}}$ . The results of the linear response parameters are classified by three columns of table 2. These columns denote

- (i) a range of  $E/N$  where  $r_{\text{BA}}$  was derived,
- (ii) and the corresponding range of mean electron energies  $\langle \varepsilon \rangle$  obtained with the MC simulation for the buffer gas.
- (iii) a figure number where  $r_{\text{BA}}$  was plotted as a function of  $E/N$ .

The  $r_{\text{BA}}$ -results have been normalized to  $k = 1\%$ . The 95% confidence interval of  $r_{\text{BA}}$  is given as the error of the experimental data. In addition, the experimental data of  $r_{N_2-C_3F_8}$  and  $r_{CO_2-C_3F_8}$  are listed in table 3.

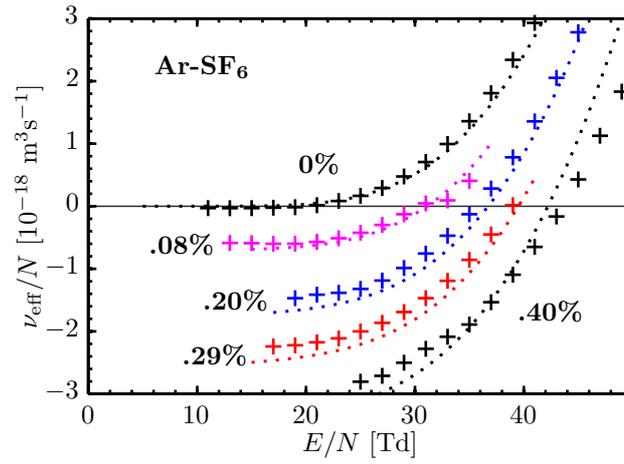
### 3.3.3. Supplemental results

- The experimental values of  $(E/N)_{\text{crit}}$  are listed in table 1.
- For  $N_2-C_3F_8$ , selected experimental results of the reduced electron mobility  $\mu N = wN/E$  are presented in figure 8.
- For selected mixtures, as indicated in table 1, the tabulated swarm parameters are given in the appendix.

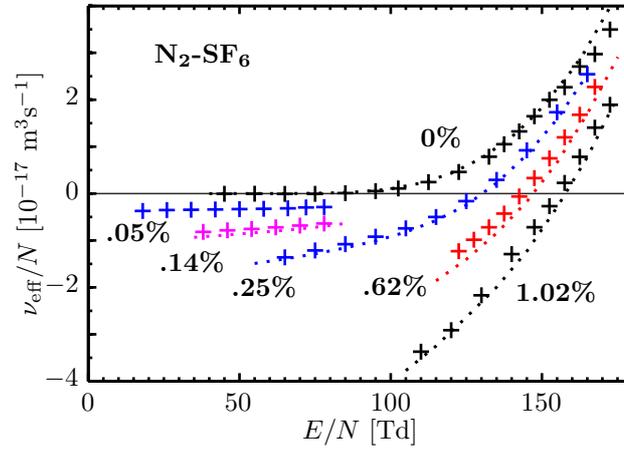
## 4. Discussion

### 4.1. Benchmark with $SF_6$

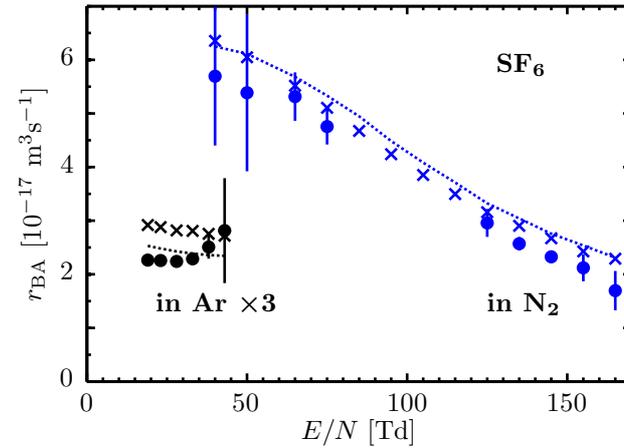
4.1.1. *Applicability of the method.* In Ar- $SF_6$  mixtures, assumption (2) may be violated because  $\sigma_a(\varepsilon \rightarrow 0 \text{ eV})$  is very large, and because the grand total cross section  $\sigma_{\text{tot}}(\varepsilon \approx$



**Figure 3.** Measured (+) and BE-calculated (·····) effective ionization rate constants  $\nu_{\text{eff}}/N$  in Ar-SF<sub>6</sub> for various mixing ratios.



**Figure 4.** Measured (+) and MC-simulated (·····) effective ionization rate constants  $\nu_{\text{eff}}/N$  in N<sub>2</sub>-SF<sub>6</sub> for various mixing ratios.



**Figure 5.** Measured (• with error |), MC-simulated (×) and BE-calculated (·····) linear response  $r_{\text{BA}}$  of  $\nu_{\text{eff}}/N$  on adding 1% SF<sub>6</sub> into Ar or N<sub>2</sub>. The data for Ar-SF<sub>6</sub> were multiplied by 3.

0.2 eV) is relatively small due to the Ar Ramsauer minimum. In  $N_2$ - $SF_6$  mixtures, assumption (2) may be violated for values of  $\varepsilon$  below the threshold of vibrational inelastic collisions with  $N_2$ . We argue that a perturbation of  $F_B$  only weakly affects  $\nu_a$  in the parameter range of the present study, because the mean electron energy  $\langle\varepsilon\rangle$  is sufficiently high, and condition (5) is met. The linear response method (4) may be applied in the  $(E/N)$ -range of the present measurements. A linear relation between  $\nu_{\text{eff}}/N$  and  $k$  is clearly observable in figure 1.

*4.1.2. Assessment of results.* At low  $E/N$ , e.g. 65 Td in  $N_2$ - $SF_6$  or 19 Td in Ar- $SF_6$ , both numerical methods give results consistent with measured values, as it is apparent from figure 1. However, at higher  $E/N$  the  $(\nu_{\text{eff}}/N)$ -results from BE and MC are significantly different from each other, probably because they employ somewhat different sets of cross sections. In the case of Ar- $SF_6$ , our measurements agree fairly well with the BE-results, see also figure 3. In the case of  $N_2$ - $SF_6$ , the measurements closely correspond to the MC-results, see also figure 4.

As one can see from figure 5, the BE- and MC-results nearly coincide on the values of  $r_{N_2-SF_6}$ . The experimental data seem to be  $\sim 5\%$  smaller, but they qualitatively reproduce the BE- and MC-values. In the case of Ar- $SF_6$ , the experimental results seem to be slightly smaller than the results of both numerical methods. We note that the cross section for the formation of  $SF_5^-$  was found to be much smaller than the ones used in the present calculations and simulations [13]. It might be necessary to adopt the cross sections from [13] in order to resolve the present small discrepancy between measurements and numerical results.

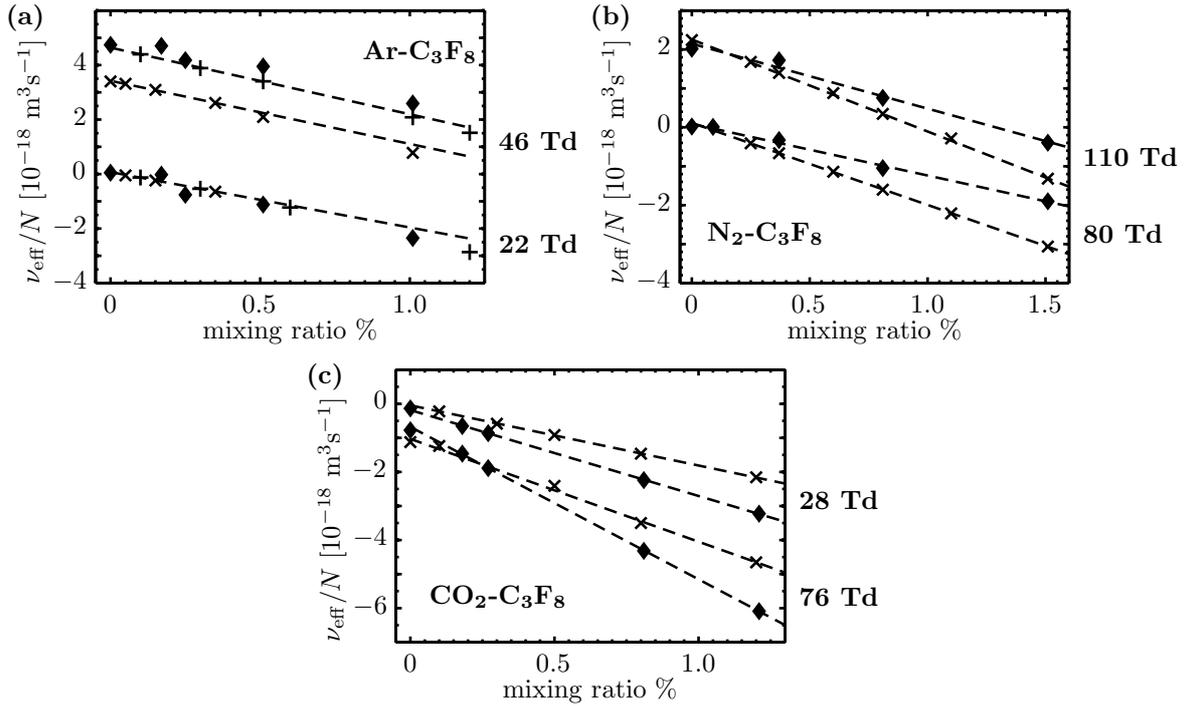
The response analysis of experimental  $(\nu_{\text{eff}}/N)$ -data (figure 5) yielded relatively small errors when the analysis was based on at least four data points. Large uncertainties of  $r_{BA}$  appeared where the response analysis was based on three data points only, i.e. for 40 and 50 Td in  $N_2$ - $SF_6$ , or for 43 Td in Ar- $SF_6$ . These  $r_{BA}$ -values with large uncertainties also seem to be qualitatively inconsistent with the reference values. It looks like the precision of experimental  $r_{BA}$ -data is adequately represented by stating the 95%-confidence interval of the linear response parameter.

## 4.2. Test of the $C_3F_8$ attachment cross section

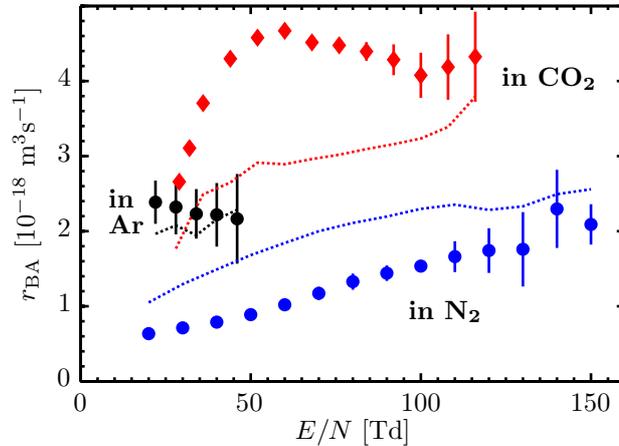
*4.2.1. Applicability of the method.* Figure 2 of [3] and figure 1 of [18] indicate a non-linear relation between  $k$  and the electron attachment rate constant  $\nu_a/N_A$ , with  $N_A$  corresponding to the partial number density of  $C_3F_8$ . It should be noted that these values  $\nu_a/N_A$  had been derived from measurements of the attachment coefficient  $\eta$ , using

$$\nu_a/N_A = \frac{\eta w_B}{N_A}, \quad (6)$$

where  $w_B$  is the electron drift velocity of the buffer gas.



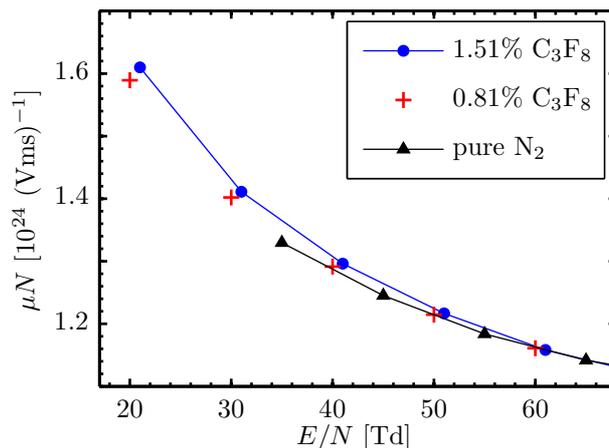
**Figure 6.** Measured ( $\blacklozenge$ ), BE-calculated (+) and MC-simulated ( $\times$ ) effective ionization rate constants in mixtures of (a) Ar- $C_3F_8$ , (b)  $N_2$ - $C_3F_8$ , and (c)  $CO_2$ - $C_3F_8$ . The lines (---) represent a linear trend.



**Figure 7.** Measured (symbols with error bars) and MC-simulated ( $\cdots$ ) linear response  $r_{\text{BA}}$  of  $\nu_{\text{eff}}/N$  on adding 1%  $C_3F_8$  into Ar ( $\bullet$ ),  $N_2$  ( $\bullet$ ) or  $CO_2$  ( $\blacklozenge$ ).

It is apparent from figure 2 of [16] and from figure 8 of the present article that  $w$  significantly increases for  $(E/N) < 40$  Td, when  $C_3F_8$  is added into  $N_2$  or Ar. We argue that the relation between  $\eta$  and  $k$  is non-linear because of the change of  $w$  with  $k$ .

In contrast, we measured  $\nu_{\text{eff}}/N$  and found a linear relation between  $\nu_{\text{eff}}/N$  and  $k$  for  $k \leq 1.5\%$  in  $N_2$ , as one can note from figure 6(b). An application of the linear response method (4) seems to be permitted for the analysis of  $N_2$ - $C_3F_8$ . In Ar buffer gas, see figure 6(a), the  $(\nu_{\text{eff}}/N)$ -values for  $k \approx 1\%$  seem to deviate from a linear trend.



**Figure 8.** Pulsed Townsend results of the reduced electron mobility in  $N_2$ - $C_3F_8$  mixtures. The lines are merely for guiding the eye.

In consequence, the linear response analysis of  $Ar$ - $C_3F_8$  was restricted to  $k \leq 0.51\%$ .

In the case of  $CO_2$ - $C_3F_8$ , assumption (2) seems to hold because both species have vibrational excitation cross sections with relatively low threshold energy. Then it is valid to apply (4).

*4.2.2. Assessment of results.* As shown in figure 7, our results for  $r_{Ar-C_3F_8}$  and the values from the MC simulation agree within the experimental uncertainty. The agreement indicates a suitable scaling of the total area of  $\sigma_a$ . The linear responses derived from the MC simulation for the  $N_2$  or  $CO_2$  buffer gases, however, are not consistent with the present experimental data. The experimental  $r_{N_2-C_3F_8}$  are much *smaller* than the MC values. On the other hand, the experimental  $r_{CO_2-C_3F_8}$  are much *larger* than the MC values.

In figure 7 the experimental data show a strong increase of  $r_{CO_2-C_3F_8}$  between 30 and 50 Td. A maximum of  $r_{CO_2-C_3F_8}$  appears near 60 Td. It is not present in the MC results. A monotonic increase of  $r_{N_2-C_3F_8}$  with increasing  $E/N$  consistently appears in the experimental and simulated results. The uncertainty of the experimental response data is particularly large in such  $(E/N)$ -ranges where strong ionization occurs. In these  $(E/N)$ -ranges the experimental errors of  $k$  or  $E/N$  can strongly influence the measurement of  $\nu_{eff}$ . In consequence, a relatively large scatter can appear in the corresponding  $(\nu_{eff}/N)$ -values. The scatter causes a large 95%-confidence interval of the linear response parameter. For  $(E/N) < 100$  Td, the precision of the experimental response data should be sufficient for testing revised attachment cross sections of  $C_3F_8$ .

## 5. Summary and conclusions

Electron swarm methods have been successfully applied for investigating the effects of small amounts of a strongly electronegative sample gas in a buffer gas. We evaluated the sensitivity of the effective ionization rate constant to changes of the mixing ratio.

**Table 3.** Linear response  $r_{BA}$  of  $\nu_{\text{eff}}/N$  on adding 1%  $C_3F_8$  into  $N_2$  or  $CO_2$ .

$E/N$ (Td)	$r_{CO_2-C_3F_8}$ ( $10^{-18}m^3s^{-1}$ )	$E/N$ (Td)	$r_{N_2-C_3F_8}$ ( $10^{-18}m^3s^{-1}$ )
28	$2.52 \pm .04$	20	$0.63 \pm .15$
32	$3.11 \pm .04$	30	$0.72 \pm .07$
36	$3.71 \pm .07$	40	$0.80 \pm .07$
44	$4.30 \pm .07$	50	$0.90 \pm .08$
52	$4.58 \pm .03$	60	$1.03 \pm .08$
60	$4.67 \pm .02$	70	$1.17 \pm .11$
68	$4.51 \pm .02$	80	$1.33 \pm .14$
76	$4.48 \pm .04$	90	$1.45 \pm .18$
84	$4.39 \pm .12$	100	$1.57 \pm .23$
92	$4.28 \pm .20$	110	$1.67 \pm .43$
100	$4.08 \pm .30$	120	$1.74 \pm .62$
108	$4.19 \pm .43$	130	$1.75 \pm .99$
116	$4.32 \pm .60$	140	$2.25 \pm .84$
		150	$2.09 \pm .51$

The analysis yielded the linear response parameters as a function of the reduced electric field strength.

Our evaluation technique was benchmarked with an analysis of the effective ionization rate constants of  $SF_6$ -mixtures. The benchmark involved the results of our own pulsed Townsend measurements, the results of a well-approved Monte Carlo swarm method, and the results of a standard solver for the two-term expanded Boltzmann equation. We found satisfactory agreement between the linear response parameters derived from the results of the three different methods.

The linear response is a useful, characteristic parameter of gas mixtures. For example, the present technique can be applied for assessing electronegative additives for gas mixtures used in high voltage insulation applications. We gave directions for an interpretation of the linear response parameters with respect to the influence of the sample gas on the electron energy distribution in the buffer gas. A connection was made between the linear response parameters and the attachment cross sections of a sample molecule.

The linear response technique was applied for testing the attachment cross section of  $C_3F_8$ . For Ar,  $N_2$  and  $CO_2$  buffer gases, the linear response was simulated using a Monte Carlo swarm method with the recommended attachment cross sections. Experimental response data have been determined from our own pulsed Townsend measurements. As far as we know, the present work is the first report on swarm parameter measurements in  $CO_2$ - $C_3F_8$  mixtures. For the admixtures of  $C_3F_8$  to Ar or  $N_2$ , our measurements of the effective ionization rate constant complement the data hitherto in the literature by expanding the range of mean electron energies covered.

The incompatibility of Monte Carlo simulations of electron attachment to  $C_3F_8$  in  $N_2$  or  $CO_2$  with the experimental data indicates the necessity to re-assess the attachment

cross sections of  $C_3F_8$ .

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**Table A1.** Bulk velocity and effective ionization rate constant of Ar.

$E/N$ (Td)	$w$ ( $10^3 \text{ ms}^{-1}$ )	$\nu_{\text{eff}}/N$ ( $10^{-18} \text{ m}^3\text{s}^{-1}$ )
11.0	10.6	$-0.03 \pm .01$
15.0	14.4	$-0.03 \pm .01$
19.0	18.0	$-0.02 \pm .01$
21.0	19.7	$0.02 \pm .01$
23.0	21.4	$0.08 \pm .01$
27.0	24.9	$0.29 \pm .01$
31.0	28.2	$0.71 \pm .01$
35.0	31.5	$1.36 \pm .02$
39.0	34.6	$2.34 \pm .03$
43.0	37.7	$3.59 \pm .05$
47.0	40.9	$5.14 \pm .06$
49.0	42.4	$5.76 \pm .07$

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## Appendix A. Tabulated swarm data

PT measurements of the bulk velocity and the effective ionization rate constant are given for selected values of the reduced electric field strength  $E/N$ , which is in units of  $1 \text{ Td} = 10^{-21} \text{ Vm}^2$ .

The precision of the data is:

- $\pm 1.5\%$  experimental uncertainty of  $E/N$ .
- $\pm 0.5\%$  statistical uncertainty of  $w$ .
- The statistical uncertainty of  $\nu_{\text{eff}}/N$  is stated in the data tables.

The data for Ar (table A1) have been remeasured in order to cover a wider ( $E/N$ )-range than our previous measurements [22].

**Table A2.** 0.20%  $SF_6$  in Ar.

$E/N$ (Td)	$w$ ( $10^3 \text{ ms}^{-1}$ )	$\nu_{\text{eff}}/N$ ( $10^{-18} \text{ m}^3\text{s}^{-1}$ )
19.0	17.9	$-1.47 \pm .01$
21.0	19.7	$-1.41 \pm .01$
23.0	22.0	$-1.38 \pm .01$
27.0	25.3	$-1.19 \pm .01$
31.0	28.2	$-0.76 \pm .01$
35.0	31.5	$-0.13 \pm .02$
37.0	33.0	$0.28 \pm .02$
41.0	36.1	$1.36 \pm .03$
45.0	39.9	$2.78 \pm .05$
47.0	41.4	$3.51 \pm .06$
49.0	43.1	$4.55 \pm .07$

**Table A3.** 0.51%  $C_3F_8$  in Ar.

$E/N$ (Td)	$w$ ( $10^3 \text{ ms}^{-1}$ )	$\nu_{\text{eff}}/N$ ( $10^{-18} \text{ m}^3\text{s}^{-1}$ )
22.0	23.0	$-1.12 \pm .01$
26.0	25.5	$-0.90 \pm .01$
30.0	28.0	$-0.47 \pm .01$
34.0	30.9	$0.12 \pm .01$
38.0	33.8	$1.03 \pm .02$
42.0	37.3	$2.31 \pm .03$
46.0	40.8	$3.95 \pm .04$
50.0	43.8	$5.56 \pm .05$
54.0	47.0	$7.55 \pm .07$

**Table A4.** 0.25%  $SF_6$  in  $N_2$ .

$E/N$ (Td)	$w$ ( $10^3 \text{ ms}^{-1}$ )	$\nu_{\text{eff}}/N$ ( $10^{-18} \text{ m}^3\text{s}^{-1}$ )
65.0	73.9	$-13.6 \pm .1$
75.0	83.5	$-12.1 \pm .1$
85.0	93.7	$-10.8 \pm .1$
95.0	104	$-9.19 \pm .04$
105	114	$-7.42 \pm .03$
115	123	$-4.99 \pm .04$
125	134	$-1.61 \pm .07$
135	144	$2.92 \pm .10$
145	155	$9.22 \pm .15$
155	165	$17.3 \pm .2$
165	176	$25.4 \pm .3$

**Table A5.** 0.81%  $C_3F_8$  in  $N_2$ .

$E/N$ (Td)	$w$ ( $10^3 \text{ ms}^{-1}$ )	$\nu_{\text{eff}}/N$ ( $10^{-18} \text{ m}^3\text{s}^{-1}$ )
20.0	31.8	$-0.61 \pm .01$
30.0	42.0	$-0.68 \pm .01$
40.0	51.6	$-0.75 \pm .01$
50.0	60.7	$-0.83 \pm .01$
60.0	69.6	$-0.92 \pm .01$
70.0	78.5	$-1.01 \pm .01$
80.0	87.6	$-1.05 \pm .01$
90.0	97.1	$-0.89 \pm .01$
100	107	$-0.36 \pm .01$
110	117	$0.76 \pm .02$
120	128	$2.72 \pm .05$
130	138	$5.75 \pm .08$
140	149	$10.4 \pm .2$
150	159	$16.7 \pm .2$

**Table A6.** 0.81%  $C_3F_8$  in  $CO_2$ .

$E/N$ (Td)	$w$ ( $10^3 \text{ ms}^{-1}$ )	$\nu_{\text{eff}}/N$ ( $10^{-18} \text{ m}^3\text{s}^{-1}$ )
20.0	60.9	$-1.15 \pm .01$
28.0	85.1	$-2.24 \pm .03$
36.0	96.9	$-3.25 \pm .03$
44.0	104	$-3.99 \pm .02$
52.0	110	$-4.57 \pm .03$
60.0	116	$-4.99 \pm .03$
68.0	121	$-4.95 \pm .02$
76.0	127	$-4.32 \pm .02$
84.0	132	$-2.83 \pm .03$
92.0	137	$-0.21 \pm .02$
100	143	$3.56 \pm .07$
108	149	$8.75 \pm .11$
116	155	$15.8 \pm .2$